

Communication Numérique

DSP théorique des codes en ligne

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<http://xymaths.free.fr/index.php?subdir=Signal>

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- 7 Code AMI

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Soit $x(t) = g(t) * a(t)$ un signal codé en ligne, avec
 $a(t) = \sum_k \alpha_k \delta(t - kT)$, et donc, $x(t) = \sum_k \alpha_k g(t - kT)$.

$$DSP(x)(f) = DSP(g)(f) \times \gamma_a(f)$$

où,

$$\gamma_a(f) = \frac{\sigma_a^2}{T} + \frac{\bar{\alpha}^2}{T^2} \Pi_{1/T}(f) + \frac{2}{T} \sum_{n=1}^{\infty} \Gamma_{\alpha}(n) \cos(2\pi n f T)$$

avec les caractéristiques statistiques de la suite (α_k) :

$$\left\{ \begin{array}{ll} \text{Moyenne :} & \bar{\alpha} = E(\alpha_k) \\ \text{Variance :} & \sigma_{\alpha}^2 = \text{Var}(\alpha_k) = E(\alpha_k^2) - \bar{\alpha}^2 = \overline{\alpha^2} - \bar{\alpha}^2 \\ \text{Auto-corrélation :} & R_{\alpha\alpha}(n) = E(\alpha_k \alpha_{k+n}) = \Gamma_{\alpha}(n) + \bar{\alpha}^2 \end{array} \right.$$

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DSP du code unipolaire NRZ

$$g(t) = V\text{Rect}_{T_b}(t) \implies \underline{|\widehat{g}(f)|^2 = V^2 T^2 \text{sinc}^2(fT_b)}$$

$$\alpha_k \in \{0; 1\}, \text{ donc, } \begin{cases} \bar{\alpha} = \frac{1}{2} \\ \sigma_\alpha^2 = \overline{\alpha^2} - \bar{\alpha}^2 = \frac{1}{2} - \left(\frac{1}{2}\right)^2 = \frac{1}{4} \\ \Gamma_\alpha(k) = 0; \forall k \geq 1 \end{cases}$$

D'où,

$$\text{DSP}(f) = \frac{V^2 T}{4} \text{sinc}^2(fT_b) + \frac{V^2}{4} \text{sinc}^2(fT_b) \Pi_{1/T_b}(f)$$

Or, $\text{sinc}(fT_b) = 0 \iff f = \frac{k}{T_b}, \forall k \in \mathbb{N}^*$

d'où, finalement,

$$\text{DSP}(f) = \frac{V^2 T}{4} \text{sinc}^2(fT_b) + \frac{V^2}{4} \delta(f)$$

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DSP du code polaire NRZ

$$g(t) = V\text{Rect}_{T_b}(t) \implies \underline{|\hat{g}(f)|^2 = V^2 T^2 \text{sinc}^2(fT_b)}$$

$$\alpha_k \in \{-1; 1\}, \text{ donc, } \begin{cases} \bar{\alpha} = 0 \\ \sigma_{\alpha}^2 = \overline{\alpha^2} - \bar{\alpha}^2 = 1 - 0 = 1 \\ \Gamma_{\alpha}(k) = 0; \forall k \geq 1 \end{cases}$$

d'où,

$$\text{DSP}(f) = V^2 T \text{sinc}^2(fT_b)$$

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DSP du code unipolaire RZ

$$g(t) = V\text{Rect}_{T_b/2}(t) \implies \underline{|\hat{g}(f)|^2 = \frac{V^2 T^2}{4} \text{sinc}^2\left(\frac{fT_b}{2}\right)}$$

$$\alpha_k \in \{0; 1\}, \text{ donc, } \begin{cases} \bar{\alpha} = \frac{1}{2} \\ \sigma_\alpha^2 = \overline{\alpha^2} - \bar{\alpha}^2 = \frac{1}{2} - \left(\frac{1}{2}\right)^2 = \frac{1}{4} \\ \Gamma_\alpha(k) = 0; \forall k \geq 1 \end{cases}$$

D'où,

$$\text{DSP}(f) = \frac{V^2 T}{16} \text{sinc}^2\left(\frac{fT_b}{2}\right) + \frac{V^2}{16} \text{sinc}^2\left(\frac{fT_b}{2}\right) \Pi_{1/T_b}(f)$$

DSP du code unipolaire RZ

$$\text{Or, } \text{sinc}\left(\frac{fT_b}{2}\right) = \begin{cases} 1 & \text{si } f = 0 \\ 0 & \text{si } f = \frac{2k}{T_b}, \forall k \in \mathbb{N}^* \\ \frac{(-1)^k}{k\pi + 1/2} & \text{si } f = \frac{2k+1}{T_b}, \forall k \in \mathbb{N}^* \end{cases}$$

d'où, finalement,

$$\text{DSP}(f) = \frac{V^2 T}{16} \text{sinc}^2\left(\frac{fT_b}{2}\right) + \frac{V^2}{16} \text{sinc}^2\left(\frac{fT_b}{2}\right) \Pi_{1/T_b}(f)$$

$$= \frac{V^2 T}{16} \text{sinc}^2\left(\frac{fT_b}{2}\right) + \frac{V^2}{16} \sum_{k \geq 1} \frac{1}{(k\pi + 1/2)^2} \delta\left(f - \frac{2k+1}{T_b}\right)$$

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DSP du code polaire RZ

$$g(t) = V \text{Rect}_{T_b/2}(t) \implies \underline{|\hat{g}(f)|^2 = \frac{V^2 T^2}{4} \text{sinc}^2\left(\frac{f T_b}{2}\right)}$$

$$\alpha_k \in \{-1; 0; 1\}, \text{ donc, } \begin{cases} \bar{\alpha} = 0 \\ \sigma_\alpha^2 = \overline{\alpha^2} - \bar{\alpha}^2 = \frac{1}{2} \\ \Gamma_\alpha(1) = -\frac{1}{4}; \Gamma_\alpha(k) = 0; \forall k \geq 2 \end{cases}$$

d'où,

$$\begin{aligned} \text{DSP}(f) &= \frac{V^2 T}{8} \text{sinc}^2\left(\frac{f T_b}{2}\right) - \frac{V^2 T^2}{8} \text{sinc}^2\left(\frac{f T_b}{2}\right) \cos(2\pi f T_b) \\ &= \frac{V^2 T}{8} \text{sinc}^2\left(\frac{f T_b}{2}\right) [1 - \cos(2\pi f T_b)] \end{aligned}$$

et finalement,

$$\text{DSP}(f) = \frac{V^2 T}{8} \text{sinc}^2\left(\frac{f T_b}{2}\right) \sin^2(\pi f T_b)$$

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DSP du code Manchester

$$g(t) = V\text{Rect}_{T_b/4}(t + T/2) + V\text{Rect}_{T_b/4}(t - T/2)$$
$$\implies \underline{|\hat{g}(f)|^2 = V^2 T^2 \frac{\sin^2\left(\frac{\pi f T_b}{2}\right)}{\pi f T_b / 2}}$$

$$\alpha_k \in \{-1; 1\}, \text{ donc, } \begin{cases} \bar{\alpha} = 0 \\ \sigma_\alpha^2 = \overline{\alpha^2} - \bar{\alpha}^2 = 1 \\ \Gamma_\alpha(1) = 0, \forall k \geq 1 \end{cases}$$

et finalement,

$$\text{DSP}(f) = V^2 T \frac{\sin^4\left(\frac{\pi f T_b}{2}\right)}{(\pi f T_b / 2)^2}$$

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DSP du code AMI

$$g(t) = V\text{Rect}_{T_b}(t) \implies \underline{|\widehat{g}(f)|^2 = V^2 T^2 \text{sinc}^2(fT_b)}$$

$$\alpha_k \in \{-1; 0; 1\}, \text{ donc, } \begin{cases} \bar{\alpha} = 0 \\ \sigma_\alpha^2 = \overline{\alpha^2} - \bar{\alpha}^2 = \frac{1}{2} \\ \Gamma_\alpha(1) = -\frac{1}{4}; \Gamma_\alpha(k) = 0 \quad \forall k \geq 2 \end{cases}$$

D'où,

$$\begin{aligned} \text{DSP}(f) &= \frac{V^2 T}{2} \text{sinc}^2(fT_b) - \frac{V^2 T}{2} \text{sinc}^2(fT_b) \cos(\pi fT_b) \\ &= \frac{V^2 T}{2} \text{sinc}^2(fT_b) [1 - \cos(\pi fT_b)] \end{aligned}$$

d'où, finalement,

$$\text{DSP}(f) = V^2 T \frac{\sin^4(\pi fT_b)}{(\pi fT_b)^2}$$